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(54) Title: BIODEGRADABLE COMPOSITES					
(57) Abstract					
A fully biodegradable fibre reinforced composite adapted for use as a medical implant which is shaped and processed by means of a resin reaction injection transfer molding process adapted for predetermining shape, physical properties and degradation profile, shaped preform and/or composition for preparation of the shaped composite, process for the production of the shaped composite comprising obtaining a shaped preform and impregnating with resin with simultaneous processing thereof, shaped composite comprising thermoplastic matrix and fibres adapted for use as a medical implant, characterised by a differential degradation of matrix with respect to fibres adapted to degrade via an intermediate shaped structure comprising residual porous matrix or residual fibre form respectively and selection of composite is made for primary growth of a preferred cell type, throughout voids created by degraded matrix or fibre respectively, according to the desired healing or reconstruction locus, the shaped composites for use as an implant in surgical reconstruction, preferably for use in reconstructive surgery of bone or in reconstructive surgery of cartilage and/or meniscus selected from cranial, maxillofacial and orthopaedic surgery for the purpose of fixation, augmentation and filling in of defects, and method for the production of a shaped product comprising preparation of set sizes, shapes and configurations, e.g. plates, screws, rivets and other fixation devices according to a 3-dimensional template wherein the template is obtained by means of preparing a 3-dimensional image of a selected feature or area for implant, generating a mold as hereinbefore defined, selecting fibre and matrix for preparation of a composite, preparing a fibre preform by introducing fibre into the mould in an effective amount and arrangement, injecting matrix and catalyst and processing thereof with subsequent removal of the mold.					

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BIODEGRADABLE COMPOSITES

The present invention relates to a biocompatible, biodegradable composite,
5 production and/or preparation thereof, for use, particularly but not exclusively,
in surgical procedures such as surgical implantation and bone fixation,
resurfacing and augmentation procedures. Additionally, it will be appreciated
that the invention may have other applications in the fields of consumer goods,
packaging, storage and transport aids given the relative rigidity and impact
10 resistance of the composite whilst also being advantageously biodegradable.

Despite numerous examples of the use of synthetic, permanent implant
materials such as acrylic polymer, silicone elastomer, ceramic polymer
composites, polymethylmethacrylate, polyethylene and porous PTFE-carbon
15 fibre composite, the reconstruction of traumatic, developmental and surgical
osseous defects is largely dependent upon an adequate supply of autogenous
(host) or allogeneic (donor) bone. Bone autograft is widely considered the best
implant material for repairing bone defects, simply because of the reduced
likelihood of rejection and concomitant immunological problems. However, the
20 amount of autogenous bone available for transplantation is limited since it has
to be taken from a part of the host's own body. Furthermore, the harvesting
operation itself carries with it the risk of post-operative complications, in some
instances this risk is of a greater magnitude than the primary procedure itself
especially if the individual has recently suffered severe trauma.

25

Common donor sites include bone material of the iliac crest, tibia, fibula and
greater trochanter. Bone itself has at least two distinct types, and selection of

bone type is dependent upon its intended implant site and function. Cortical bone (that is the outer layers) is selected for its strength and mechanical support, whilst cancellous bone (that is the more spongy form) autografts are used to promote lattice formation and rapid bone regeneration. Autografts of either 5 and/or both types have been used extensively and successfully used in oral and maxillofacial surgery for restoration of the periodontium and correction of mandibular and maxillary defects.

Rapid and extensive vascularisation of the graft is important for survival of the 10 bone graft and supply of appropriate nutrients and the like to cells. However, problems have been encountered using autograft bone due to shrinkage of the graft material itself and partial and variable resorption of the osteons and hence restricted regenerative capacity of new bone. It is of note that whilst allografted (where bone is transplanted between two individuals – often from cadaveric 15 donors with specimens being kept in bone banks) bone avoids the potential risks of a harvesting operation it offers a potentially unlimited material in banked form. Nevertheless, banking of bone is a complex procedure involving extensive, time consuming and expensive procedures:- donor selection, screening, procurement and storage. Moreover, the possible transmission of 20 diseases such as Creutzfeldt-Jacob or AIDS raises significant and potentially lethal problems with its use. Several years may be required for reabsorption and replacement of allograft by new bone and the antigenic activity of non-host bone is a serious disadvantage compared with autografts. As a consequence, the search for suitable alternatives to host and donor bones has intensified.

25

It is known to provide bioceramics of calcium phosphate, typically these are in the form of biodegradable tricalcium phosphate and hydroxyapatite products.

Furthermore such bioceramics display advantages of biocompatibility, osteoconductive capability and chemical similarity to mineralised bone matrix which results in direct bonding to bone. Consequently they satisfy most of the essential criteria for successful bone grafting. However, significantly, 5 bioceramics do not appear to induce pronounced osteogenesis. Furthermore the inherent hardness of bioceramics render them difficult to shape thus bioceramics have limited use within an animal skeleton as the material cannot be readily shaped to the defect. Moreover, the rigidity is also a disadvantage as the healing progresses because the rigid plate causes stress shielding around the 10 fracture site and as a consequence the bone is not subject to the normal force induced remodelling at the site of fracture closure. This can be a serious problem if the fracture plate is removed, with the underlying bone being unable to handle the forces acting upon it and a refracture may result. Additionally and disadvantageously bioceramics also remain in the repair site for extended 15 periods, typically more than one year.

Additionally it is known to use mixtures of collagen/ceramic/marrow, with the aim of replicating the organic matrix/mineral phase/osteogenic cell structure of bone. However, such mixtures have a limited capability in that they are useful 20 only in fracture repair partially due to the paste-like quality of the mixture and hence difficulty in accurate and permanent placement and retention of the material at the site requiring repair.

It is recognised that a synthetic, re-absorbable polymeric implant could 25 overcome many of the problems associated with the prior art not least the supply difficulties, long reabsorption time of the implant and bone union times vis-à-vis the implant; moreover the novel implant would immediately provide

an advantage to current practices.

Notably, there is currently no successful biocompatible and/or biodegradable material for reconstructive surgery of bone in the face and skull and associated 5 areas of disfigurement. Surgery to the face and skull following trauma, injuries, correction of congenital or acquired deformities and ablation of tumours can leave areas of bone discontinuity and/or distortion. Untreated bony defects can cause marked functional disability and disfigurement, furthermore disfigurement can be psychologically damaging and cause a great deal of 10 personal and/or familial anxiety. Reconstructive surgery is an extremely important area of modern surgery and advanced techniques can lead to remarkable results. The current surgical procedures involve the replacement of bone structures with means as herein before described in addition to metal plates such as titanium alloys, cobalt-chromium alloys, and sculptured 15 polyethylene for replacement of tissue sections and/or bony defects. The use of metal plates however has become increasingly less popular due to interference with medical imaging, consequently an investigator is unable to analyse the state of tissue (eg brain) or the like covered by said plate. Effectively the plate prevents imaging of tissue behind the plate. Moreover 20 metallic fracture plates are not ideal for maxillofacial skull or long bone reconstruction. The delicate nature of facial bone requires miniature fixation screws, causing associated problems of obtaining a reliable joint. The complex facial geometry necessitates special plates and techniques, particularly in areas such as the orbital floor. Furthermore metallic plates can in some cases be 25 visual and palpable below the skin and in many cases these plates have to be removed requiring a second operation with all the associated risks and costs. The surgical approach required to retrieve plates can be a complex and lengthy

procedure. In other bones, plates are routinely removed, an inevitable cause of morbidity.

5 All biomaterials currently commercially available for cranio-facial and maxillofacial reconstructive surgery have significant problems including Proplast (polyethylene), Silastic (silicone), hydroxyapatite and bioactive glass granules. Problems with these and other materials include migration of the implant, formation of cold abscesses, lack of colour compatibility, lack of dimensional stability and difficulty in shaping of the material to "fit" the defect.

10 Bone from allograft and autograft sources are also difficult to sculpture to a specific implant site and furthermore sculpting of bone can destroy/damage the living cells.

15 The ideal biomaterial for maxillofacial and other types of bony/cartilaginous reconstruction will have numerous properties. It should be biocompatible, capable of facilitating revascularisation and cell growth providing a framework to guide the new bone development. The material needs to be sterile, malleable, storable and affordable. It could also act as a carrier mechanism for osteogenic proteins. A high initial stiffness will allow primary union followed by gradual 20 resorption and reduction in stiffness corresponding with the healing bone's ability to serve in a load bearing capacity. Ideally the material should be easily processed into complex shaped components. With the use of CT patient scan data this creates the possibility of producing accurate tailored implants for elaborate reconstructive surgery.

25 The ability to vary the degradation rate of biocompatible relatively short length -polyesters such as polylactide and polyglycolide by copolymerization, and to

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control molecular weight, crystallinity and morphology has made these two materials natural candidates for bone repair and are the most promising materials in the development phase. However they remain far from ideal.

5 Poly- ϵ -caprolactone (PCL) is a relatively long -polyester hydrocarbon chain thermoplastic ($T_m = 60^\circ\text{C}$) having a low elastic modulus which mitigates against its use in bone implants without some structural reinforcement. The characteristics of PCL increases its relative permeability with respect to other -polyesters and thus PCL has been exploited as a vehicle for diffusion

10 controlled delivery of low molecular weight (MW 400) drugs and has been used in the area of contraceptive therapeutics.

US 4,655,777 and US 5,108,755 disclose composites comprising PCL matrix reinforced with certain biodegradable fibres for improved retention of yield

15 strength and modulus with time under degrading conditions. In US 5,108,755 is disclosed a need for composites providing prompt clearance from the system without premature compromising degradation. In US 4,655,777 is disclosed matrix reinforced with biodegradable long, continuous fibres for increased strength. The composites are prepared using conventional processing routes.

20 Nevertheless there is a need for a method to provide shaped composites suited for the above mentioned applications in the form of pins, plates or custom shaped implants, for which the existing processes are lacking in convenience and versatility. There is moreover a need for shaped composites having

25 improved performance as bone repair materials.

It is therefore a first object of the invention to provide a biocompatible

composite for use in transplant surgery, bony resurfacing or the fixation of fractures and/or tissue scaffolding.

It is yet a further object of the invention to provide a biocompatible composite
5 for use in crano-facial or maxillo-facial surgery, some applications of orthopaedic surgery such as replacement of bone/cartilage/meniscus.

It is yet a further object of the invention to provide a biocompatible composite with differential biodegradation properties.

10

It is yet a further object of the invention to provide a biocompatible composite which may be moulded to any size or shape that it is desired to implant/reconstruct.

15 It is yet a further object of the invention to provide a biocompatible composite which is fully biodegradable.

It is yet a further object of the invention to provide a biodegradable composite to replace glass-reinforced polypropylene or the like in the various industries.

20

We have now unexpectedly found that by use of a specific process for processing composites for the presently envisaged applications in shaped form, excellent results in terms of processing convenience and product quality are obtained. We have moreover found that degradation may be predetermined in 25 manner to provide custom composites adapted for implant/reconstructive surgery with excellent recovery time. We have also found that the process and products are suited for new applications further enhancing the versatility of the

technology.

In its broadest aspect the invention provides a fully biodegradable fibre reinforced composite adapted for use as a medical implant which is shaped and 5 processed by means of a resin reaction injection transfer moulding process adapted for predetermining shape, physical properties and degradation profile.

More specifically the invention relates to a fully biodegradable fibre reinforced shaped composite obtained by *in situ* processing of a thermoplastic matrix 10 precursor in a shaped preform of fibres.

Use as medical implant may include any known use for example selected from cranial, maxillofacial and orthopaedic surgery for the purpose of fixation, augmentation and filling in of defects.

15

The novel composites are of any desired 3 dimensional geometry which may be complex, having chemical and mechanical properties comparable to those of composites obtained using conventional bulk polymerisation processes. Preferably the composites are shaped in the form of pins, plates, meshes, 20 screws, rivets and/or custom shaped implants to fit the contour of the area to be constructed and to secure the device, optionally made to a range of sizes for more general use or the manufacture of plates and fixation devices to support bone during healing.

25 For example a custom implant for augmentation of filling of defects may comprise associated devices for fixation. Restoration of bone or other biological tissues such as cartilage, may be envisaged.

In situ processing is partial or substantial polymerisation from a composition comprising (co)monomers and/or oligomers of a biodegradable thermoplastic polymer matrix in a shaped fibre preform of fibre-reinforcement into which matrix is injected in manner to retain predetermined fibre distribution, 5 orientation and/or fraction, and composite shape.

A shaped fibre preform as hereinbefore defined may be any presentation of fibres in a suitable tool, mould or the like adapted for impregnation with polymer or polymer precursors to provide a composite having irregular shape. 10 The shaped fibre preform preferably enables a predetermined regular, irregular and/or otherwise profiled fibre distribution.

Fibres may be any natural or synthetic loose, aligned, knitted or woven material or fabric having length and direction selected for desired mechanical properties. 15 Short fibres which are up to 10^2 times greater in length than diameter may be employed where only moderate load bearing strength is required, or long continuous fibres which are $10^2 - 10^4$ times greater in length than diameter may be employed where high load bearing strength is required.

20 It has been found that the composition processed *in situ* provides accuracy, ease and convenience of handling and shaping to provide a shaped composite, without compromising the excellent properties in terms of modulus and strength, provided by the fibre reinforcement and matrix. The composition may moreover be selected to provide polymer matrix of desired molecular weight, 25 adapted for the required degradation profile, irrespective of concerns over ease of impregnation of fibres, for example with use of high molecular weight, high viscosity polymers.

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Preferably the composite is obtained by *in situ* polymerisation of a composition comprising a shaped fibre preform as hereinbefore defined of continuous or long fibres in intimate admixture with an effective amount of liquid or solid (co)monomers or oligomers.

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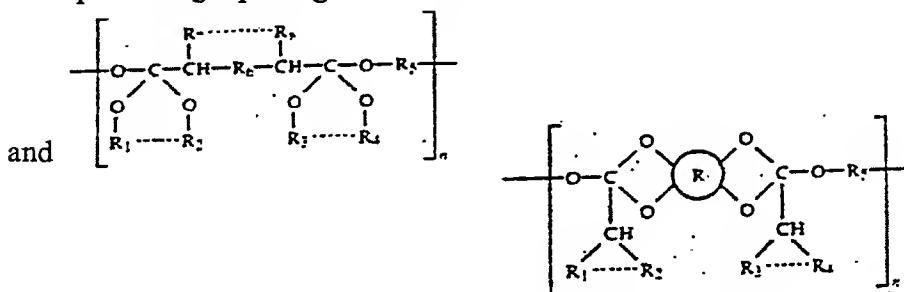
The composites of the invention are found to be ideally suited for the intended uses by virtue of their versatility to provide high quality high strength implants adapted in novel manner for biocompatibility and cell growth by controlled or differential degradation.

10

The polymer matrix and fibres may comprise any biodegradable, biocompatible polymer, bioglass and the like having the desired properties. Suitable materials are disclosed in US 5,108,755, US 4,655,777, US 5,674,286, WO 95/07509 the contents of which are incorporated herein by reference.

15

In particular matrix materials may be selected from acrylics, polyesters, polyolefins, polyurethanes, silicon polymers, vinyl polymers, halogenated hydrocarbons such as teflon, nylons, proteinaceous materials, and copolymers and combinations thereof. For example matrix may be selected from poly ortho esters formed by reaction of a multifunctional ketene acetal with a polyol, for example having repeating units of formula



wherein R is independently selected from H and hydrocarbon,

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or from polylactides (DL- or L-lactide), polylactic acids (PLA, PLLA, PDLLA), epsilon caprolactone, polycaprolactone (PCL), polyglycolic acid (PGA), polypropylene fumarate, polycarbonates such as polymethyl carbonate and polytrimethylenecarbonate, polyiminocarbonate, polyhydroxybutyrate, 5 polyhydroxyvalerate, polyoxalates such as poly(alkylene)oxalates, polyamides such as polyesteramide and polyanhydrides described by K W Leong et al, J. Biomed. Res. Vol 19, pp941-955 (1985), and copolymers and combinations thereof in particular poly (DL-lactide-co-glycolide) (DL-PLG), poly (L-lactide-co-glycolide), copolymers of polyhydroxybutyrate and polyhydroxyvalerate.

10

Preferably the matrix is selected from polymers and copolymers of aliphatic polyesters such as poly- ϵ -caprolactone and/or biocompatible derivatives and/or analogues thereof.

15 In particular the fibre reinforcement is selected from a plurality of suitable, synthetic and/or natural fibres selected from ceramics such as beta-tricalcium phosphate and phosphate free calcium aluminium (Ca-Al), bioglasses such as the glass form of calcium phosphate, calcium metaphosphate (CMP) and calcium sodium metaphosphate (CSM), mixtures of silica, sodium oxide, 20 calcium oxide and phosphorus pentoxide, suture material and any of the above polymeric materials. For example the fibres may be constructed of phosphate and/or polyglycolide such as polyglycolic acid (PGA) and/or polylactide such as polylactic acid (PLA) and/or copolymer (Vicryl mesh), polydioxanone (PDS) and/or bioabsorbable glass (favoured for its significant reinforcing effect but 25 also because it may act as a buffer for the acidic degradation by-products) or the like. Particular advantages are obtained when the fibres are 10^2 to 10^4 times greater in length than in diameter.

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In a preferred embodiment the invention provides a shaped composite, comprising polycaprolactone and/or biocompatible derivatives and/or analogues thereof or precursors thereof; and long, or directional continuous, fibre-reinforcement.

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In a further aspect the invention provides a shaped preform and/or composition for preparation of a shaped composite as hereinbefore defined.

10 In a further aspect the invention provides a process for the production of shaped composite as hereinbefore defined comprising obtaining a shaped preform as hereinbefore defined and impregnating with resin as hereinbefore defined with simultaneous processing thereof.

15 The composite of the invention is preferably obtained by polymerisation using a modified resin transfer moulding technique. Resin transfer moulding (RTM) is a composite manufacturing technique normally used with thermosetting resins ⁽¹⁾. A reactive liquid resin is injected into a tool cavity containing a dry fibre preform. The resin wets out and infiltrates into the fibre bundles and upon curing produces a composite thermoset material.

20

RTM is preferably adapted as a manufacturing technique for biocompatible biodegradable polymer matrices such as PCL as hereinbefore defined. The novel process allows the production of complex shaped bioabsorbable composite materials. Preferably fibre fractions and directions are controlled
25 The low pressure process requires only economic lightweight tooling and injection equipment allowing us to produce thermoplastic components without the normal expense of conventional injection moulding tooling and machinery.

A mould for preparing a preform as hereinbefore defined may be constructed of any desired natural or synthetic material having temperature resistance in excess of the processing temperature to be employed in processing the composite. Suitable materials for constructing the mould include steel, 5 aluminium and the like which may be coated with release agents as known in the art, for example wax, poly vinyl alcohol, silicone based agents and the like, or is constructed entirely from materials have release properties, for example is machined from PTFE.

10 The mould may be of any desired construction suitable for injection of resin into a preformed fibre bundle or the like. For example the mould may comprise a portion having a machined cavity and a further portion having inlet and outlet ports for introduction of resin and release of volatile and bleed excess resins.

15 The composite may be obtained by polymerisation by suitable means, preferably by heating or by addition of an initiator or catalyst which may be present in or added to the composition *in situ*.

A composite comprising PCL for example is suitably obtained by cationic 20 polymerisation for example using an organometallic catalyst such as organozinc, preferably diethylzinc. The catalyst may be adapted to coordinate to a reactive group such as carbonyl on caprolactone resulting in cleavage of a bond and cation formation which can then add to a further caprolactone resulting in the growth of the polymer chain. The method results in well defined 25 polymers with high molecular weight and narrow polydispersities (<2). The lack of branching by this method also gives higher crystallinity and higher T_m, and therefore superior material properties, which are thought to be more appropriate

in the biodegradation process.

It is a particular advantage that the process which can be carried out at low pressure and using lightweight tooling, as described above, may be adapted for 5 preparing shaped composites non-industrially with use of a small scale or portable moulding unit for immediate use, dispensing with the need to commission in advance from an industrial manufacturing source. This has clear benefits in terms of customising shaped composites to be produced as a one-off product.

10

Surprisingly, we have found that PCL is highly biocompatible with osteoblasts. Moreover, unlike most biodegradable polymers, which tend to degrade via bulk hydrolysis to monomer constituents with a sudden breakdown of the material resulting in large amounts of degradation products lowering the surrounding pH 15 and producing inflammatory/foreign body responses, PCL bioerodes at the surface, a phenomenon which advantageously allows for rapid replication of bone cells and remodelling of bone during biodegradation. Typically osteoblasts infiltrate into the matrix and allow the bone to form around the fibres, thus providing good implant bonding and maintaining biological and 20 mechanical integrity. Furthermore the use of PCL as a matrix in a long fibre composite material should give significant scope for the tailoring of mechanical and degradation properties by varying the matrix molecular weight and the fibre orientation and fraction.

25 The invention of the application also concerns the serendipitous finding that a PCL matrix, reinforced with long fibres, biodegrades at a slower rate and differentially so that during bone remodelling, osteoblasts migrate into the PCL

matrix and allow the bone matrix to form around the fibre, thus maintaining mechanical and biological integrity. Consequently the observed preferential biodegradation of the matrix material allows osteoblasts to infiltrate and differentiate into osteocytes and to grow around the long fibres, the fibres 5 themselves biodegrade only after the bone has substantially formed and regrown. Therefore, the development of a totally bioabsorbable long fibre composite material allows a two stage degradation to occur with a differential rate of degradation between the components such that one degrades first leaving a void or scaffold structure of the other which would be absorbed at a later 10 stage.

In a further aspect of the invention there is provided a shaped composite comprising thermoplastic matrix and fibres adapted for use as a medical implant, obtained by any desired conventional or non-conventional process, 15 wherein the composite is characterised by a differential degradation of matrix with respect to fibres adapted to degrade via an intermediate shaped structure comprising residual porous matrix or residual fibre form respectively and selection of composite is made for primary growth of a preferred cell type, throughout voids created by degraded matrix or fibre respectively, according to 20 the desired healing or reconstruction locus.

According to this aspect of the invention, fibres are contemplated within the composite not only for strengthening reinforcement, as known in the art, but also or alternatively are contemplated as a means to generate a void structure for 25 in growth of cells, blood vessels and the like, or to generate a residual scaffold for attachment and growth of cells.

16

Accordingly the composite is suitably selected for primary growth of cells selected from bone, cartilage, tissue and the like cells to create a supporting structure of live bone or cartilage or a live vascular structure within the partially degraded composite, adapted for further growth of remaining cells types for 5 total integration as a functioning live system.

The differential degradation composites of the invention provide the continuity of mechanical integrity and the intended preferential degradation mechanism in which the matrix or fibres degrade only after bone or vascular formation 10 respectively within the composite matrix.

According to this aspect of the invention, matrix and fibre material differ in chemical composition, either in terms of nature of material or molecular weight thereof or other feature affecting degradation rate. The matrix or fibres may 15 moreover comprise a combination of materials whereby a differential degradation is exhibited both within and between the matrix and/or fibre. Degradation rate of a material may be determined by means known in the art and selection of respective materials having a desired differential may be made. It is convenient to classify materials according to slow, medium and fast 20 degradation rates whereby selection of material having the appropriate rate may be made together with any other desired physical, mechanical and chemical properties for the intended use.

Either matrix or fibre may be adapted for primary degradation, with the other 25 being adapted for secondary degradation. Preferably matrix is selected for primary degradation when it is desired to implant for reconstruction of bone or cartilage or the like. Preferably fibre is selected for primary degradation when

it is desired to implant for reconstruction of soft tissue, muscle or the like.

The nature of fibres may also be selected to provide a desired void or residual structure specifically adapted to promote a desired vascular/muscle or 5 bone/cartilage structure. For example a parallel aligned fibre preform of continuous long fibres will create a different void or residual structure to that of a felt or knitted or woven mat of short non-aligned fibres, which may be specifically selected to mimic a living structure or to provide a scaffold on which a living structure can most efficiently establish itself.

10

A shaped composite as hereinbefore defined may be coated with or associated with or have embedded therein or be impregnated with an appropriate therapeutic agent. Preferably the therapeutic agent is an antibiotic and/or a growth promoter and/or a vitamin supplement which aids implantation, growth 15 and take of said curable composition.

A shaped composite as hereinbefore defined may be coated with or associated with or have embedded therein or be impregnated with a selected population of host and/or compatible donor cells. Preferably the cells are bone derived and/or 20 cartilage derived and/or collagen derived. The selection of said cells is dependent on the intended implant site and inclusion of said cells is intended to aid implantation, growth and take of said curable composition at the site of implantation.

25 Furthermore, we have inventively discovered a means for matching the implant geometry exactly to the patient, by use of medical imaging and liquid moulding of the composite to a dimensionally accurate surgical feature construct.

According to a further aspect of the invention there is provided a shaped composite as hereinbefore defined for use as an implant in surgical reconstruction, ideally said implant is for use in reconstructive surgery of bone such as the bone of the face and/or skull or in reconstructive surgery of cartilage and/or meniscus.

It will be appreciated by those skilled in the art of surgical reconstruction that the use of the composite of the invention is not intended to be limited to use in bony areas of the face and skull but is intended to be used on any part of the body of an animal or human that has ossification and/or cartilage and/or meniscus that requires surgical reconstruction and so the examples referred to herein are not intended to limit the scope of the application. Additionally it will be appreciated that reconstructive surgery is intended to include cosmetic surgery and surgery for aesthetic purposes.

15

The composite may moreover be impregnated with cells as hereinbefore defined.

In a further embodiment the composite may be used as a template for in vivo tissue production using bioengineering techniques as known in the art. In this embodiment the impregnation may be with cells as hereinbefore defined, inductive proteins, therapeutic substances and the like, and the composite is then adapted for introduction into a living host, such as the human or animal body or a part thereof, and subsequently harvesting the composite in partial or substantially impregnated and/or degraded state and reimplanting in a locus for reconstructive surgery.

Implant may be into muscle for attachment and growth of living cells, with subsequent harvesting at the time of definitive surgery, for example in cranial, maxillofacial, orthopaedic and the like surgery as hereinbefore defined to provide bone, cartilage and the like.

5

According to a further aspect of the invention there is provided a method for the production of a shaped product comprising comprising preparation of set sizes, shapes and configurations, eg plates, screws, rivets and other fixation devices according to a 3 dimensional template wherein the template is obtained by 10 means of preparing a 3 dimensional image of a selected feature or area for implant, generating a mould as hereinbefore defined, selecting fibre and matrix for preparation of a composite as hereinbefore defined, preparing a fibre preform by introducing fibre into the mould in an effective amount and arrangement, injecting matrix and catalyst as hereinbefore defined and 15 processing thereof with subsequent removal of the mould.

Preferably the method comprises :

preparing a three dimensional image whose shape is determined by a 20 plurality of co-ordinates provided by medical imaging of a selected feature or area of a patient, ideally a feature or area complementary to or symmetrical with a feature or area to be replaced and/or restructured;

(ii) production of custom made, patient specific devices by passing data 25 collected from medical imaging to a translating system which interprets said data and generates information for transferring said information to a rapid prototyping system typically a stereolithography system for generating a mould;

20

liquid moulding a product to a specified size and shape, by introducing a suitable amount of matrix resin as hereinbefore defined for example: caprolactone and/or biocompatible derivatives and/or analogues thereof; and fibres as hereinbefore defined, for example long, or directional continuous, 5 fibre-reinforcement; and catalyst and/or initiator into said mould under conditions that favour in-situ polymerisation of matrix;

(iv) curing said composite by appropriate means;

10 (v) removing the mould from a cured shaped product; and, optionally preparing said shaped product for introduction into a recipient by appropriate means.

15 In this work, catalysed caprolactone monomer is injected into a tool cavity to produce test plaques of PCL. Specimens with different molecular weights have been produced and the physical and biocompatibility characteristics of this in-situ polymerised material compared to commercially available PCL. The effect of gamma sterilisation has also been investigated as this is the most likely 20 sterilisation procedure to be used for such implants. A cell culture system with bone cells derived from craniofacial bone cells (CFC) has been used to assess the biocompatibility of the PCL material. Finally, totally bioabsorbable long fibre reinforced composite materials have been manufactured using this in-situ polymerisation technique using both knitted and woven Vicryl meshes produced 25 from a polylactic acid/ polyglycolic acid (PLA/PGA) copolymer.

The invention will now be described, by way of example only, with reference

to the following figures, wherein:-

(i) Figure 1 represents a block schematic representation of the process of the invention.

5

(ii) Figure 2 represents a front cross-sectional view of the apparatus employed in in-situ polymerisation of polycaprolactone.

Figure 3 represents a perspective, partial cross-sectional view of a machined
10 PTFE rectangular cavity mould.

Figure 4 - GPC curves showing molecular weight distribution;
unsterilised PCL 75; b) gamma sterilised PCL 75.

15 (v) Figure 5 - Tensile modulus Vs molecular weight for unsterilised and gamma sterilised PCL □: unsterilised *in-situ* polymerised PCL, O: gamma sterilised *in-situ* polymerised PCL, X unsterilised CAPA 650 (measured value), • : gamma sterilised CAPA 650 (measured value), ■ : unsterilised CAPA 650 (Solvay value).

20

Figure 6 - H^1 NMR spectra for PCL 50.

Figure 7 - H^1 NMR spectra for CAPA 650.

25 viii) Figure 8 - Reflection IR spectra; a) CAPA 650 b) PCL 50

ix) Figure 9 shows a cross-sectional view of knitted Vicryl mesh/PCL

22

composite showing the knitted mesh to be fully integrated with the PCL matrix material. Note also the twisted, knitted structure of the Vicryl mesh.

5 x) Figure 10 shows a cross-sectional woven Vicryl mesh/PCL composite showing the woven structure of the Vicryl mesh.

xi) Figure 11 shows individual Vicryl fibres fully wet out and encapsulated within the PCL matrix material.

10 10 Figure 12 shows an Alamar Blue assay of CFC on PCL of different molecular weights after 48 hours.

MATERIALS AND METHODS

Modelling Curable Composition

15

With reference to Figure 1, there is shown an individual's face (1) wherein area 2A represents a feature or area to be surgically treated. Area 2B represents a complementary feature or area, typically symmetrical with the feature or area to be treated. In order to match the implant geometry closely to the patient, 20 medical imaging (3) such as CT and/or MRI and/or NMR (or MRI) scanners are used to provide three dimensional data of a complementary feature or area. In the instance where a complementary feature or area does not exist, or is not suitable, data derived from a compatible or average image may be used in the working of the invention. Optionally the medical imaging data may be mirror 25 imaged so as to provide an image of appropriate hand.

Medical imaging data is then processed along arrow B in a conventional manner

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so as to provide data in the correct form for rapid prototyping (4). Rapid prototyping is a means by which moulds for liquid moulding can be made, directly or indirectly, and it will be appreciated by those skilled in the art of providing an implant that this particular procedure is not intended to limit the scope of the application but merely to provide a means by which a preformed mould (5) may be produced. Following along process D, the closed mould (5) in which a preform of synthetic and/or natural fibres is placed along with an appropriate amount of caprolactone is then subjected to in-situ polymerisation (6). (This process will be described in greater detail in the following text.)

10 Subsequent to polymerisation and curing of the polycaprolactone material the mould is removed along process E so as to provide a shaped product (7) which upon appropriate deflashing and preparation is implanted following process F into the appropriate position of an individual's face (1).

15 In this way it is apparent that the process of the invention requires multiple integrated steps, the exact nature of which is not intended to limit the scope of the application but merely provide examples of the ways and means of providing a shaped product for transplantation from the composite of the invention.

20

For more general use a series of sized moulds may be used to provide a range of preformed implants, plates, fixation devices and the like as hereinbefore defined.

25

In-situ polymerisation of polycaprolactone**Monomer Preparation**

ε-Caprolactone monomer (Solvay Interox, Widnes, UK) was purified by
5 distillation under reduced pressure over freshly powdered calcium hydride. The
reaction apparatus is outlined in figure 2. Distilled caprolactone monomer dried
over molecular sieves was charged into a 500 ml round bottom five-necked
flask fitted with a Teflon blade stirrer, an inlet for dry nitrogen gas, a
thermocouple probe, a rubber septum inlet and a outlet pipe. Attached in line
10 with the outlet pipe was a machined PTFE rectangular cavity mould with a
peripheral nitrile O-ring seal with the mould outlet attached to a vacuum pump.
Initiator in the form of 1,4 butane-diol contained within low molecular weight
(Mw 4000) powdered PCL (Capa 240, Solvay Interox) was added in the
quantity required to give the desired molecular weight as detailed in table 1.

15

Polymer and Composite Production

The mixture was heated to 80°C with an oil bath and stirred under nitrogen for
2 h. 500 ppm di-ethyl zinc ((C₂H₅)₂Zn) catalyst as a 15 wt.-% solution in
20 toluene was added with a syringe via the septum inlet followed immediately by
vigorous stirring for 30 s during which the mould cavity and reaction vessel
were evacuated to 0.2 bar absolute in order to degas the monomer. The stirring
was stopped and after a further 30s - 60 s degassing the pressure in the vessel
was increased to ambient, the mould inlet tube pushed down into the monomer
25 and the nitrogen pressure used to inject the catalysed monomer into the mould
cavity. Upon filling the cavity the inlet and outlet pipes were clamped shut and
the mould heated in an oven to 120°C for 18 h. Finally the mould was allowed

25

to cool to room temperature and the polymerised PCL moulding removed from the mould. Two moulds were used, one with cavity dimensions 240 x 130 x 3 mm used for producing material for tensile and biocompatibility test specimens and a smaller one 80 x 30 x 3 mm used for producing the composite specimens.

5 The fibre preforms consisted of 12 layers of either woven or knitted Vicryl mesh (polyglactin 910 from Ethicon, Edinburgh) cut to fit the mould cavity and vacuum dried over molecular sieves for 12 h at 120°C. The knitted material tends to deform at temperature so this was dried while clamped between aluminium plates.

10

Comparative sample preparation

PCL (CAPA 650, Solvay Interox) was obtained in 3mm thick compression moulded sheets. This is a commercially available PCL with a nominal Mn of 15 50,000 and was used as a bench mark material to compare with the samples produced using our *in-situ* manufacturing technique.

Tensile test specimens were prepared by machining the PCL sheets into rectangular strip specimens 40 x 10 x 3 mm using a high speed fly cutter. Disc 20 specimens for biocompatibility testing were produced using a 10 mm diameter circular punch. Both tensile and biocompatibility test specimens were sterilised with gamma radiation using an irradiation does of 27.8 kGy.

Having regard to the above the following procedure is a summary of the 25 procedure used to polymerise caprolactone in-situ:-

(i) Construct the preform of dry synthetic and/or natural fibres to the

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required length and/or geometry, and place in mould.

(ii) Heat the mould to a suitable temperature below the melting/degredation point of the fibres and purge with dry nitrogen, or the like.

5

(iii) Distil the caprolactone monomer or oligomer at reduced pressure over a suitable anhydrous salt such as calcium hydride so as to remove impurities.

10 (iv) Heat the caprolactone monomer to a selected temperature under reduced pressure so as to remove any entrained air.

15 (v) In a vessel purged with nitrogen, add a stoichiometric quantity of an appropriate initiator such as (1,4-butanediol) and 50-250 ppm of a suitable catalyst such as (diethyl zinc in toluene) using syringes which have been dried and nitrogen-purged. Mix thoroughly.

20 (vi) Using a peristaltic pump and thoroughly-dried silicone tubing, pump the reaction mixture into an evacuated mould containing the preform of biodegradable fibres. When filled, seal entry and exit points and heat to 100° to 140° for an appropriate period until polymerisation has taken place (typical times appear to be 5 hours).

Deflash and tidy up the moulding prior to treatment and/or use for implantation.

25 Measurements

Gel permeation chromatography (GPC Polymer Laboratories) was performed

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to determine the molecular weight distributions. Mixed D columns calibrated with polystyrene narrow standards (Polymer Laboratories PS-1) were used with 100 mg of polymer dissolved in 5mL of chloroform as the mobile phase.

5 Tensile modulus was measured with a Instron 1195 tensile testing machine using a clip-on electrical extensometer with a 10 mm gauge length a 5 kN load cell and a cross head speed of 1 mm/min.

Reflection infra-red spectroscopy was undertaken using a Perkin-Elmer system
10 2000 FT-IR spectrometer.

H^1 NMR of the sample and comparison recorded in CDCL_3 , on a Bruker 300MHz FT-NMR using tetramethyl silane as the internal standard to assess similarity of the materials via their electronic structure.

15 Differential scanning calorimetry (DSC) was used to determine the melting temperature (T_m) and crystallinity of the PCL specimens. A Dupont Instruments 910 DSC calibrated with Indium was used with a starting temperature of -80°C and a heating rate of $10^\circ\text{C}/\text{min}$.

20 Biocompatibility Testing
Cell Culture

25 Cranio facial osteoblast-like cells (CFC) were derived from bone fragments of skull from a 14 month old female. This method was based on that described by Robey and Termaine ⁽²⁾. Bone fragments were cut into small pieces, no more than 5mm in diameter, rinsed in sterile phosphate-buffered saline (PBS) to

remove blood and debris, then plated out in 35mm diameter tissue culture plastic dishes (Falcon, Becton Dickinson Labware, Franklin Lakes, NJ, USA).

Bone chips were cultured in complete Dulbecco's Modified Eagle Medium (DMEM) supplemented with 10% fetal bovine serum (FBS), 1% L-glutamine,

5 1% non-essential amino acids (NEAA), 2% Hepes buffer, 2% penicillin/streptomycin (all Gibco, Paisley, UK) 150 μ g/l L-ascorbic acid (Sigma, Poole, UK) and 1 μ g/ml Fungizone (Gibco) and incubated at 37°C in 5% CO₂ humidified atmosphere. Bone chip cultures were screened daily and culture medium changed every two days.

10

After several days, seams of bone cells formed around the edges of the bone chips and cells then began to attach to the tissue culture plastic and spread out.

Within 2-3 weeks sufficient bone cells had grown out from the bone chips to be cultured alone. The bone chips were removed from culture and digested in

15 0.02% trypsin/0.03% collagenase in PBS incubated at 37°C for 20 minutes, rotated continually. The bone chips were discarded and the supernatant was centrifuged at 1200 rpm for 5 minutes to produce a cell pellet which was then resuspended in DMEM and centrifuged again to rinse off the trypsin/collagenase solution. The resulting cell pellet was resuspended and
20 replated in 25 cm² tissue culture plastic flask (Falcon). Cells were grown to confluence and then passaged with 0.02% trypsin/0.1M Herpes in PBS. Cells were characterised as osteoblast-like by morphological, ultrastructural and biochemical techniques, primarily by the expression of alkaline phosphatase, a marker of osteoblastic phenotype.

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Biocompatibility

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Cells were seeded onto gamma-irradiated and non-irradiated polymer discs of different molecular weights. Two sets of polymers discs were used: 10 mm diameter discs were used for cell activity and morphology; and 8mm diameter discs for morphological assessment only. Tissue culture plastic or Thermanox®
5 discs were used as an example of an optimum material and copper discs as an example of a material of poor biocompatibility. The non-irradiated polymers and the copper discs were sterilised by rinsing in ethanol. For statistical significance 3 replicate samples were seeded for each type of material, along with 3 unseeded (blank) materials. Cells were seeded at a concentration of
10 40,000 cells per well in a 48 well plate and cultured for 48 hours.

Alamar Blue Assay

The Alamar blue assay (Serotec, UK) demonstrates the metabolic activity of
15 cells by detection of mitochondrial activity. Cells incorporate the indicator dye that is reduced and excreted as a fluorescent product. Medium was removed from wells, cells rinsed in Earle's Balanced Salt Solution (EBSS) then 500µl of a 1:20 Alamar Blue:Hank's Balanced Salt Solution (HBSS) added to each well. Plates were incubated at 37°C for one hour, the solution removed to a fresh
20 plate and 100µl of each solution read on cytofluor (PerSeptive Biosystems) at 535nm emission, 590nm absorbance. Blank values were extracted from experimental values to eliminate background readings.

Statistics

25

Mean values and standard deviations (SD) were computed for three replicates per sample. The analysis of variance (ANOVA) was calculated along with

30

Tukey-Kramer multiple comparison test to compare gamma-irradiated or non-irradiated samples of different molecular weights. Student's t-test was used to compare gamma irradiated and non-irradiated samples of the same molecular weights.

5

Toluidine Blue Staining

Cells were rinsed several times in PBS, fixed in 1.5% gluteraldehyde in 0.1M phosphate buffer for 30 minutes, rinsed with PBS and stained with 1%
10 Toluidine Blue in 0.05M phosphate buffer for 5 minutes. This solution was removed, cells were rinsed and covered with PBS and could then be photographed under the dissecting microscope.

Scanning Electron Microscopy (SEM)

15

After toluidine blue staining, cells were fixed in osmium tetroxide for 30 minutes. Thereafter specimens were dehydrated through a series of ascending alcohols (50%-100%) dried in Hexamethyldisilazane (HMDS) and left to air dry before sputter coating with gold. Samples were then viewed in a Philips 501B
20 SEM.

Results

Molecular Weight Distribution

25 Table 2 gives the measured molecular weights and polydispersities of both the unsterilised and gamma sterilised samples. Significant differences exist between the theoretical Mn and the measured value however the PCL does

show a range of molecular weights increasing in the correct order. Measuring definitive molecular weights of PCL is difficult due to the lack of a PCL standard for calibration. To obtain a more accurate figure would require the use of solution viscosity techniques. However the results do show some interesting 5 trends, in particular the reduction in Mn and the increase in Mw giving a greater Pd for the gamma sterilised samples. Figure 4 shows a comparison of the GPC curves for the unsterilised and gamma sterilised PCL 75 highlighting the broadening of the peak due to the increase in low molecular weight material. Hence it is likely that the gamma radiation is breaking some of the longer 10 polymer chains.

Tensile Modulus

Figure 5 details the variation in tensile modulus of the PCL with molecular 15 weight and the effects of gamma sterilisation upon the tensile modulus. Tensile modulus decreases with increasing molecular weight and there is a notable decrease in tensile modulus after gamma sterilisation. This is also the case for the CAPA 650 reference material which, interestingly, has a lower tensile modulus than the material produced using the *in-situ* polymerisation technique. 20 The measured value of tensile modulus for the unsterilised CAPA 650 material is within 2% of the value given in the Solvay Interox literature ²².

NMR and IR Spectra

25 Figures 6, 7 and 8 shows the H¹ NMR spectra for both the PCL 50 and CAPA 650 material. The spectra show OCH₂ at 4.1; CH₂ - C = O at 2.3 and the hydrocarbon section at 1.3-1.8 ppm. The infra-red spectra show a carbonyl at

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~ 1750 associated with the carbonyl in the backbone of the polymer. Both NMR and IR data agree with the samples of standard polymer indicating the material to be of the same type.

5 DSC Results

Results from the DSC testing are given in table 3. The T_m and crystallinity values are within the range expected for PCL and agree with the data given by Solvay however repeating the tests for both unsterilised and gamma sterilised 10 CAPA 650 material did not give highly repeatable results.

PCL/Vicryl Composites

Figures 9, 10 and 11 are SEM micrographs of the composite materials. 15 Clearly visible are the knitted and woven structures of the Vicryl mesh. Figure 11 shows a cross section of one of the yarns from the knitted composite material with the individual fibres fully encapsulated by PCL demonstrating the success of the technique for wetting out and infiltrating the fibre tows.

20 Biocompatibility

Biocompatibility of CFC on PCL of different molecular weights, both gamma-irradiated and non-irradiated, was assessed by measuring cell activity and viewing cell morphology on the polymer surface after 48 hours incubation. On 25 TCP cells attached and spread, forming a confluent layer after 48 hours. Cells were arranged in a swirling pattern, individual cells had a long, thin, spindly morphology. Cells attached and spread with good morphology on PCL of

different molecular weights. On PCL 25-100 cells had a good morphology similar to that seen on TCP. There was complete cell coverage on 8mm diameter discs but there was not always a completed covering of cells on the surface of 10mm diameter discs. The topography of the surface was not always consistent and this may have some bearing on the cell attachment and spreading, and thus activity. If grooves were present on the surface, cells aligned along them. If there was a rough surface the cells did not attach. Holes were present on the surface of some of the polymer discs, cells appear to grow round them or span across them but did not grow into them. On CAPA 650, where the surface was very smooth with some holes in it, cells grew in stellar groups with an extremely flat morphology, much more so than on TCP or PCL 25-100. There was no cell attachment on the copper discs.

Cell activity was assessed by the Alamar Blue assay as shown in Figure 12. 15 There was no significant difference in cell activity on non-irradiated PCL of different molecular weights and CAPA 650. All samples had significantly lower activity than TCP and significantly higher than copper and blank polymers, with the exception of PCL 50. Cell activity was not significantly different for gamma-irradiated PCL 75, 100 and CAPA 650, all lower than TCP 20 and higher than copper or blank polymer. On gamma irradiated PCL 25 and 50 very few cells had attached to the surface and consequently, the cell activity was significantly lower than on PCL 75, 100 and CAPA 650 and not significantly different to copper or blank polymers. There was no significant difference between cell activity and gamma-irradiated and non-irradiated PCL 75, 100 and 25 CAPA 650. Activity on gamma-irradiated PCL 25 and 50 was significantly lower than on non-irradiated PCL 25 and 50.

Discussion

Initial investigations into the development of this novel *in-situ* polymerisation technique for PCL have produced excellent results. GPC, NMR and IR analysis 5 has proved the material to have similar properties to a commercially available PCL material used as a benchmark.

Results from the tensile testing show the *in-situ* polymerised material to have a tensile modulus which is dependant upon molecular weight. The tensile 10 modulus decreases with molecular weight. In all cases except for the gamma sterilised PCL 100 material the *in-situ* polymerised PCL had a higher tensile modulus than the gamma sterilised CAPA 650 indicating that with our novel manufacturing technique we can obtain a tensile modulus greater than or comparable to our benchmark material.

15 Results from the IR and NMR analysis indicate that the *in-situ* polymerised material is of a similar chemical composition to the CAPA 650 material. GPC analysis has indicated that we can obtain similar or greater molecular weights to our benchmark material with particularly narrow molecular weight 20 distributions.

Biocompatibility results show that the CFC cells will attach and spread on PCL of different molecular weights, although this depends somewhat on the surface 25 topography of the discs. Different surface topographies were due to the different machined finish on the upper and lower PTFE mould surfaces and the ground surface finish used on the compression moulding platens for the CAPA 650 material. There was no difference in cell activity on gamma-irradiated or

non-irradiated polymers with the exception of PCL 25 and 50.

Using this *in-situ* polymerisation technique as a variant of RTM to produce totally absorbable long fibre composite materials has produced encouraging 5 results. The Vicryl fibres appear to be well wet out and encapsulated within the PCL matrix giving a two phase material. Due to their low modulus the Vicryl fibres are having little reinforcing effect, however, the use of a higher modulus bioabsorbable glass fibre will allow us to control the material mechanical properties. The use of such a low pressure liquid moulding technique should 10 allow the fabrication of patient specific implants made from low cost tooling produced directly from CT scan data using rapid prototyping techniques.

Conclusions

15 A novel manufacturing process for PCL has been developed based upon RTM, an established technique for producing composite materials using thermosetting matrices. Preliminary comparisons of the physical and biocompatibility properties of the PCL material produced using this *in-situ* polymerisation approach compared with a commercially available PCL material (CAPA 650) 20 have produced encouraging results. NMR and IR analysis show that the chemical composition of the *in-situ* polymerised material is that of PCL. GPC analysis has demonstrated that the material can be produced with a variable molecular weight and a narrow molecular weight distribution. Tensile testing results indicate a slightly higher tensile modulus for the *in-situ* polymerised 25 material compared to the CAPA 650. The effect of sterilisation by gamma irradiation has been investigated producing a broader molecular weight distribution and slight reduction in tensile modulus.

In-vitro biocompatibility of both the *in-situ* polymerised PCL and CAPA 650 material has been assessed using osteoblasts derived from human craniofacial bone cells. The material is highly biocompatible with these cells which will 5 attach and spread on both the irradiated and non-irradiated PCL and CAPA 650. The main factor influencing cell behaviour seems to be the surface topography of the polymer samples.

Long fibre composite materials have been produced using both woven and 10 knitted Vicryl meshes. SEM micrographs show the fibre to be fully wet-out and encapsulated by the PCL matrix material.

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15 Rudd, C. D., Kendall, K.N., Long, A. C., Mangin, C.E. Liquid moulding technologies. Woodhead Publishing 1997.

2. Biodegradable CAPA Thermoplastics. CAPA 650 data sheet. Solvay Interrox.

CLAIMS

1. A biodegradable fibre reinforced composite adapted for use as a medical implant which is shaped and processed by means of a resin reaction injection transfer molding process adapted for predetermining shape, physical properties and degradation profile.
2. Fibre reinforced shaped composite according to claim 1 obtained by *in situ* processing of a thermoplastic matrix precursor in a shaped preform of fibres.
3. Composite according to claim 1 or claim 2 having 3 dimensional geometry which may be complex, preferably in the form of pins, plates, meshes, screws, rivets and/or custom shaped implants, optionally made to a range of sizes.
4. Composite according to any of Claims 1 to 3 wherein processing is partial or substantial polymerisation from a composition comprising (co)monomers and/or oligomers of a biodegradable thermoplastic polymer matrix in a shaped fibre preform of fibre-reinforcement into which matrix is injected in manner to retain predetermined fibre distribution, orientation and/or fraction, and composite shape.
5. Composite according to any of Claims 1 to 4 wherein a shaped fibre preform is a presentation of fibres in a regular, irregular or profiled fibre distribution in a tool, mould or the like adapted for impregnation with polymer or polymer precursors to provide a composite having irregular shape.

6. Composite according to any of Claims 1 to 5 wherein fibres are up to 10^2 times greater in length than diameter or long continuous fibres which are 10^2 – 10^4 times greater in length than diameter.

7. Composite according to any of Claims 1 to 6 wherein matrix material is selected from acrylics, polyesters, polyolefins, polyurethanes, silicon polymers, vinyl polymers, halogenated hydrocarbons such as teflon, nylons, proteinaceous materials, and copolymers and combinations thereof, preferably 5 from poly ortho esters formed by reaction of a multifunctional ketene acetal with a polyol, for example having repeating units of formula

and

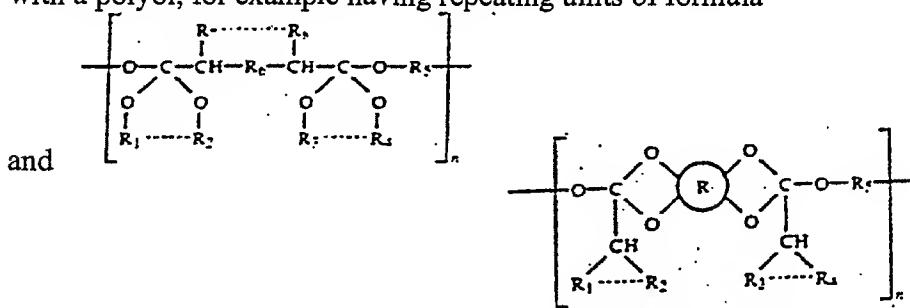
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wherein R is independently selected from H and hydrocarbon, or from polylactides (DL- or L-lactide), polylactic acids (PLA, PLLA, PDLLA), polycaprolactone (PCL), polyglycolic acid (PGA), polypropylene fumarate, polycarbonates such as polymethyl carbonate and polytrimethylenecarbonate, polyiminocarbonate, polyhydroxybutyrate, polyhydroxyvalerate, polyoxalates such as poly(alkylene)oxalates, polyamides such as polyesteramide and polyanhydrides, and copolymers and combinations thereof in particular poly (DL-lactide-co-glycolide) (DL-PLG), poly (L-lactide-co-glycolide), copolymers of polyhydroxybutyrate and polyhydroxyvalerate,

8. Composite according to Claim 7 wherein the matrix is selected from



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polymers and copolymers of aliphatic polyesters, preferably poly- ϵ -caprolactone and/or biocompatible derivatives and/or analogues thereof.

9. Composite according to any of Claims 1 to 8 wherein the fibre reinforcement is selected from ceramics such as beta-tricalcium phosphate and phosphate free calcium aluminium (Ca-Al), bioglasses such as the glass form of calcium phosphate, calcium metaphosphate (CMP) and calcium sodium metaphosphate (CSM), mixtures of silica, sodium oxide, calcium oxide and phosphorus pentoxide, suture material and any of the polymeric materials as defined in Claim 8, preferably phosphate and/or polyglycolide such as polyglycolic acid (PGA) and/or polylactide such as polylactic acid (PLA) and/or copolymer (Vicryl mesh), polydioxanone (PDS) and/or bioabsorbable glass.
10. Shaped preform and/or composition for preparation of a shaped composite as hereinbefore defined in any of Claims 1 to 9.
11. Process for the production of shaped composite as hereinbefore defined in any of Claims 1 to 9 comprising obtaining a shaped preform as hereinbefore defined and impregnating with resin as hereinbefore defined with simultaneous processing thereof.
12. Process according to Claim 11 wherein a mold is constructed of steel, aluminium or a formable mould material suitable for prototype tooling, optionally coated with release agents selected from wax, poly vinyl alcohol, silicone based agents or is machined from PTFE.
13. Process according to any of Claims 11 or 12 wherein polymerisation is

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by heating or by addition of an initiator or catalyst which may be present in or added to the composition *in situ*.

14. Process according to Claim 13 wherein polymerisation is cationic using an organometallic catalyst

15. Shaped composite comprising thermoplastic matrix and fibres adapted

5 for use as a medical implant, wherein the composite is characterised by a differential degradation of matrix with respect to fibres adapted to degrade via an intermediate shaped structure comprising residual porous matrix or residual fibre form respectively and selection of composite is made for primary growth of a preferred cell type, throughout voids created by degraded matrix or fibre 10 respectively, according to the desired healing or reconstruction locus.

16. Composite according to Claim 15 wherein fibres comprise means to generate a void structure for in growth of cells, blood vessels and the like, or to generate a residual scaffold for attachment and growth of cells.

15

17. Composite according to Claim 15 or Claim 16 wherein cells for primary growth are selected from bone, cartilage, tissue and the like cells to create a supporting structure of live bone or cartilage or a live vascular structure within the partially degraded composite, adapted for further growth of remaining cells 20 types for total integration as a functioning live system.

18. Composite according to any of Claims 15 to 17 wherein matrix and fibre material differ in chemical composition, either in terms of nature of material or molecular weight thereof or other feature affecting degradation rate.

19. Composite according to any of Claims 15 to 18 wherein the matrix or fibres comprise a combination of materials whereby a differential degradation is exhibited both within and between the matrix and/or fibre.

5

20. Composite according to any of claims 15 to 19 wherein matrix is selected for primary degradation when it is desired to implant for reconstruction of bone or cartilage or the like or fibre is selected for primary degradation when it is desired to implant for reconstruction of soft tissue, muscle or the like.

10

21. Composite according to any of Claims 15 to 20 wherein fibres are selected to provide a desired void or residual architecture specifically adapted to promote a desired vascular/muscle or bone/cartilage structure.

22. Shaped composite according to any of Claims 1 to 9 or 15 to 21 which is coated with or associated with or has embedded therein or is impregnated with an appropriate therapeutic agent, preferably an antibiotic and/or a growth promoter and/or a vitamin supplement.

23. Composite according to any of Claims 1 to 9 or 15 to 22 which is coated with or associated with or has embedded therein or is impregnated with a selected population of host and/or compatible donor cells, preferably bone derived and/or cartilage derived and/or collagen derived.

24. Shaped composite according to any of Claims 1 to 9 or 15 to 23 for use as an implant in surgical reconstruction, preferably for use in reconstructive surgery of bone or in reconstructive surgery of cartilage and/or meniscus.

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selected from cranial, maxillofacial and orthopaedic surgery for the purpose of fixation, augmentation and filling in of defects.

25. Composite according to Claim 24 for use as a template for in vivo tissue
5 production using bioengineering techniques by means of impregnation with cells, inductive proteins, therapeutic substances and the like, wherein the composite is then adapted for introduction into a living host, such as the human or animal body or a part thereof, and for subsequently harvesting the composite in partial or substantially impregnated and/or degraded state and reimplanting
10 in a locus for reconstructive surgery.

26. Composite according to any of Claims 24 and 25 wherein implant is into muscle for attachment and growth of living cells.
15 27. Method for the production of a shaped product comprising a composite according to any of Claims 1 to 9 or 15 to 26, the method comprising preparation of set sizes, shapes and configurations, eg plates, screws, rivets and other fixation devices according to a 3 dimensional template wherein the template is obtained by means of preparing a 3 dimensional image of a selected
20 feature or area for implant, generating a mold as hereinbefore defined, selecting fibre and matrix for preparation of a composite as hereinbefore defined, preparing a fibre preform by introducing fibre into the mould in an effective amount and arrangement, injecting matrix and catalyst as hereinbefore defined and processing thereof with subsequent removal of the mold.

25

28. Method according to Claim 27 comprising

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- (i) preparing a three dimensional image whose shape is determined by a plurality of co-ordinates provided by medical imaging of a selected feature or area of a patient, ideally a feature or area complementary to or symmetrical with a feature or area to be replaced and/or restructured;

5 (ii) production of custom made, patient specific devices by passing data collected from medical imaging to a translating system which interprets said data and generates information for transferring said information to a rapid prototyping system typically a stereolithography system for generating a mould;

10 (iii) liquid moulding a product to a specified size and shape, by introducing a suitable amount of matrix resin as hereinbefore defined, preferably caprolactone and/or biocompatible derivatives and/or analogues thereof, and fibre, preferably long, or directional continuous, fibre-reinforcement; and catalyst and/or initiator into said mould under conditions that favour in-situ polymerisation;

15 (iv) curing said composite by appropriate means;

(v) removing the mould from a cured shaped product; and, optionally

20 (vi) preparing said shaped product for introduction into a recipient by appropriate means.

FIGURE . 1 .

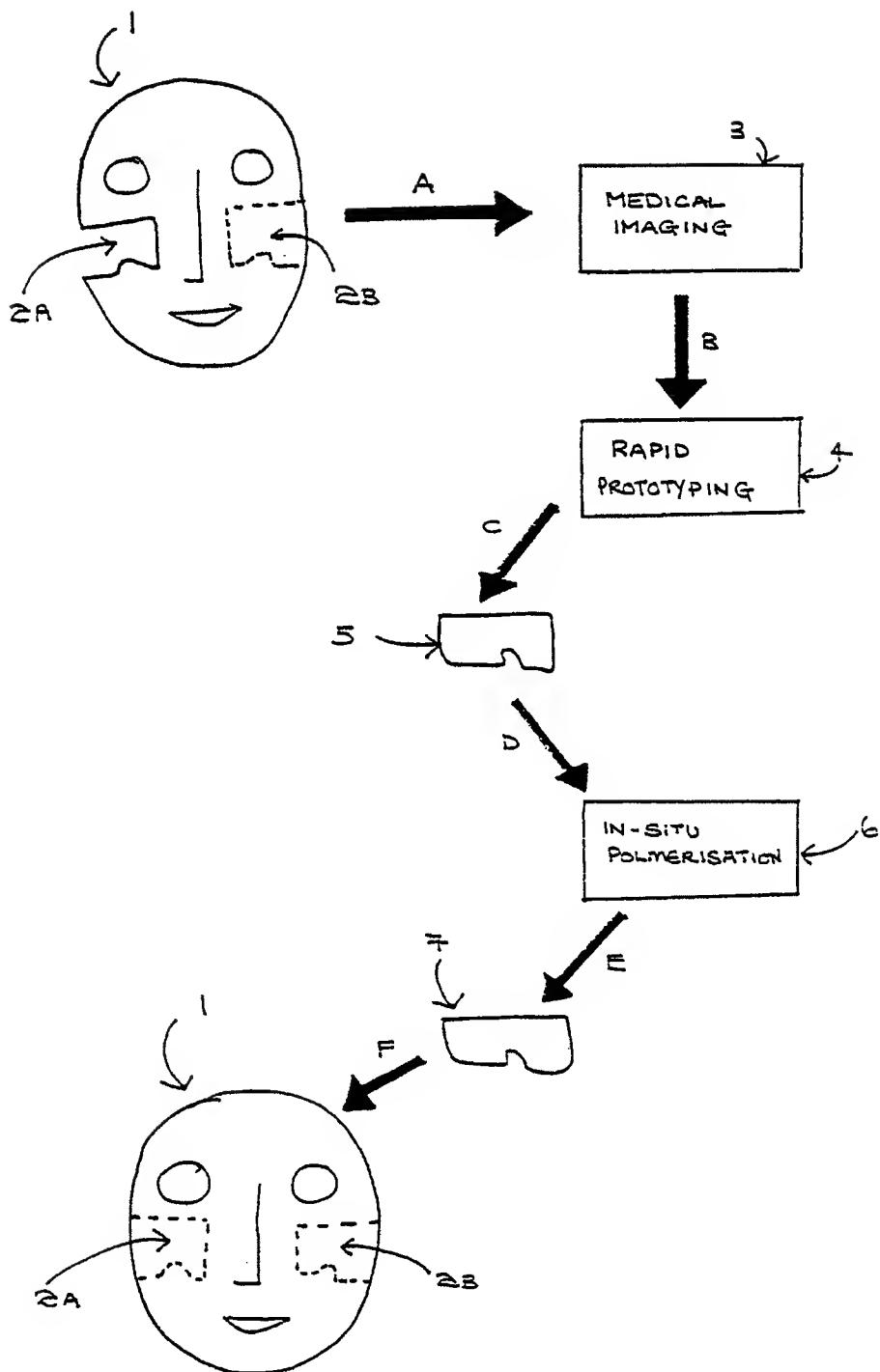


FIGURE . 2 .

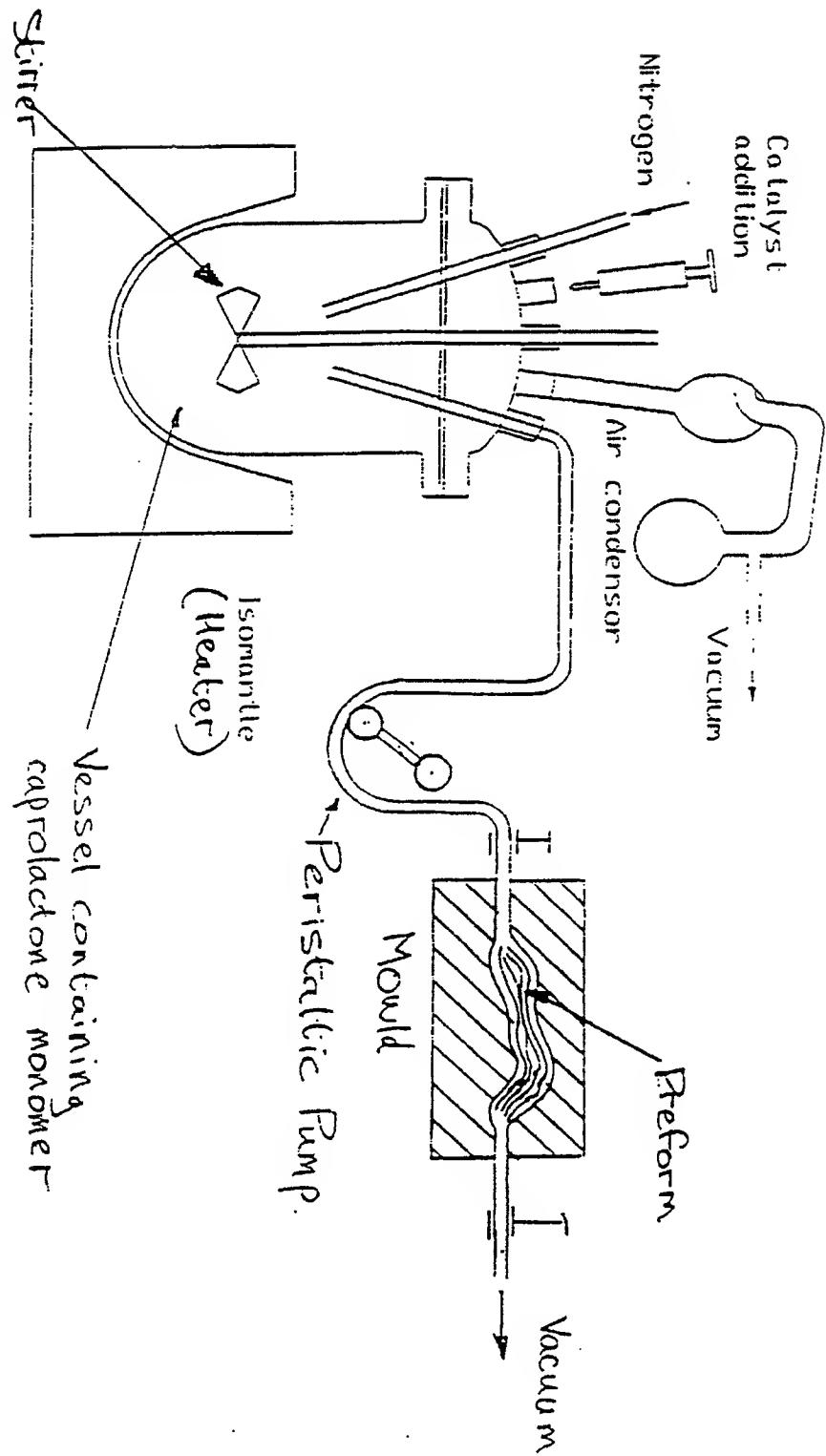


Figure 3

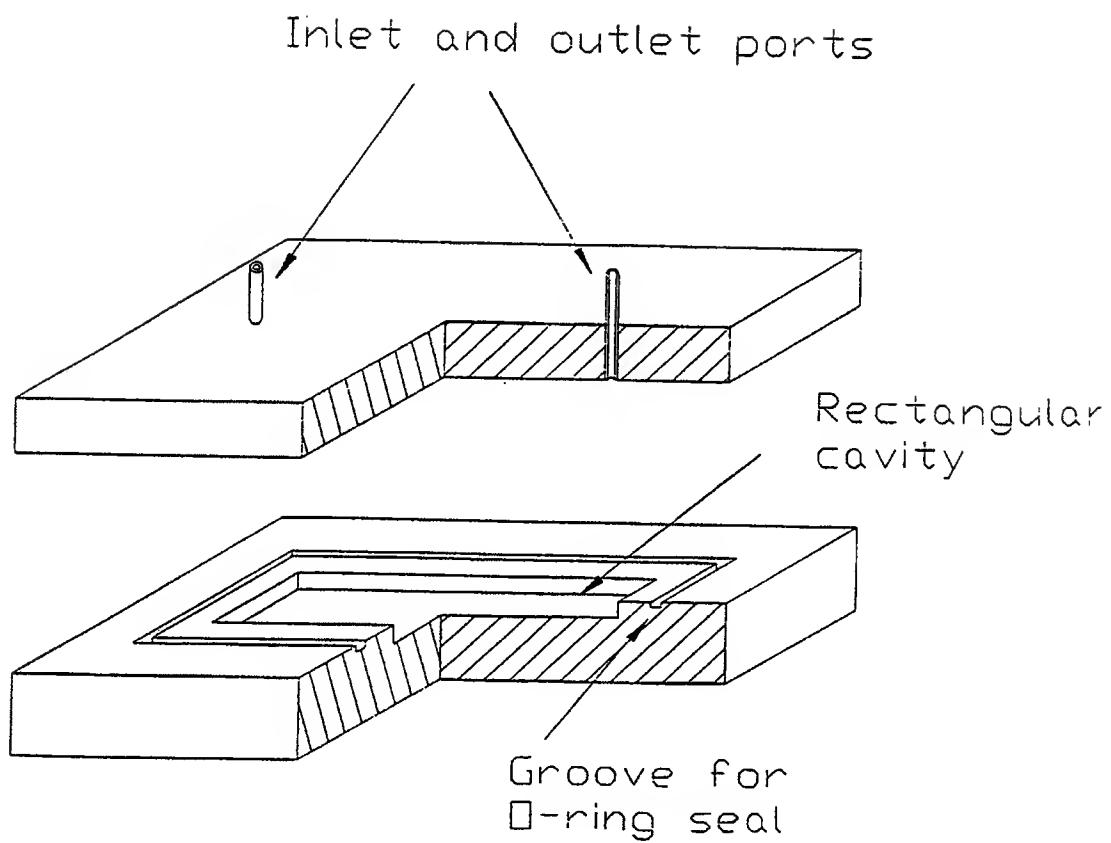


Figure 4

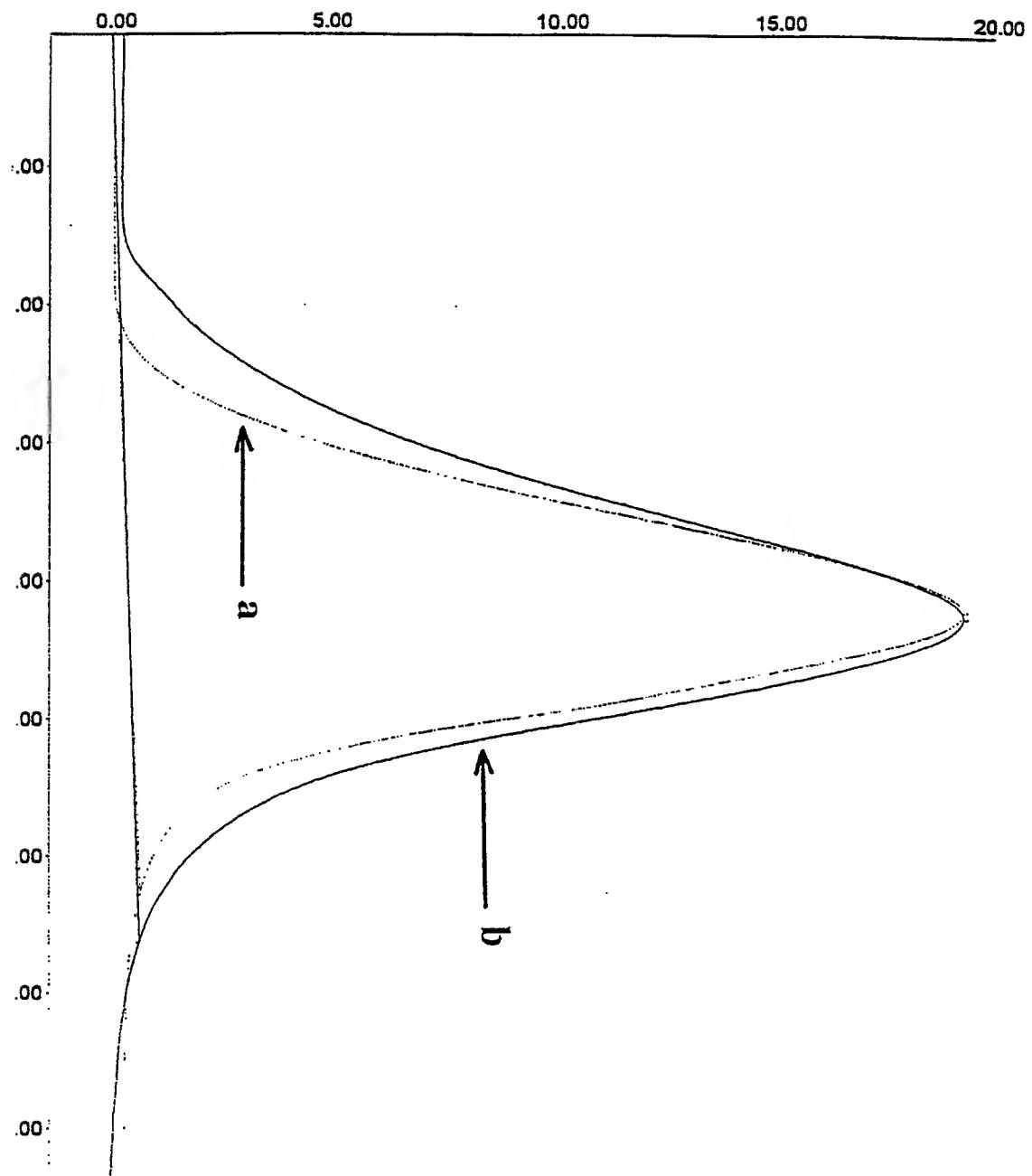


Figure 5

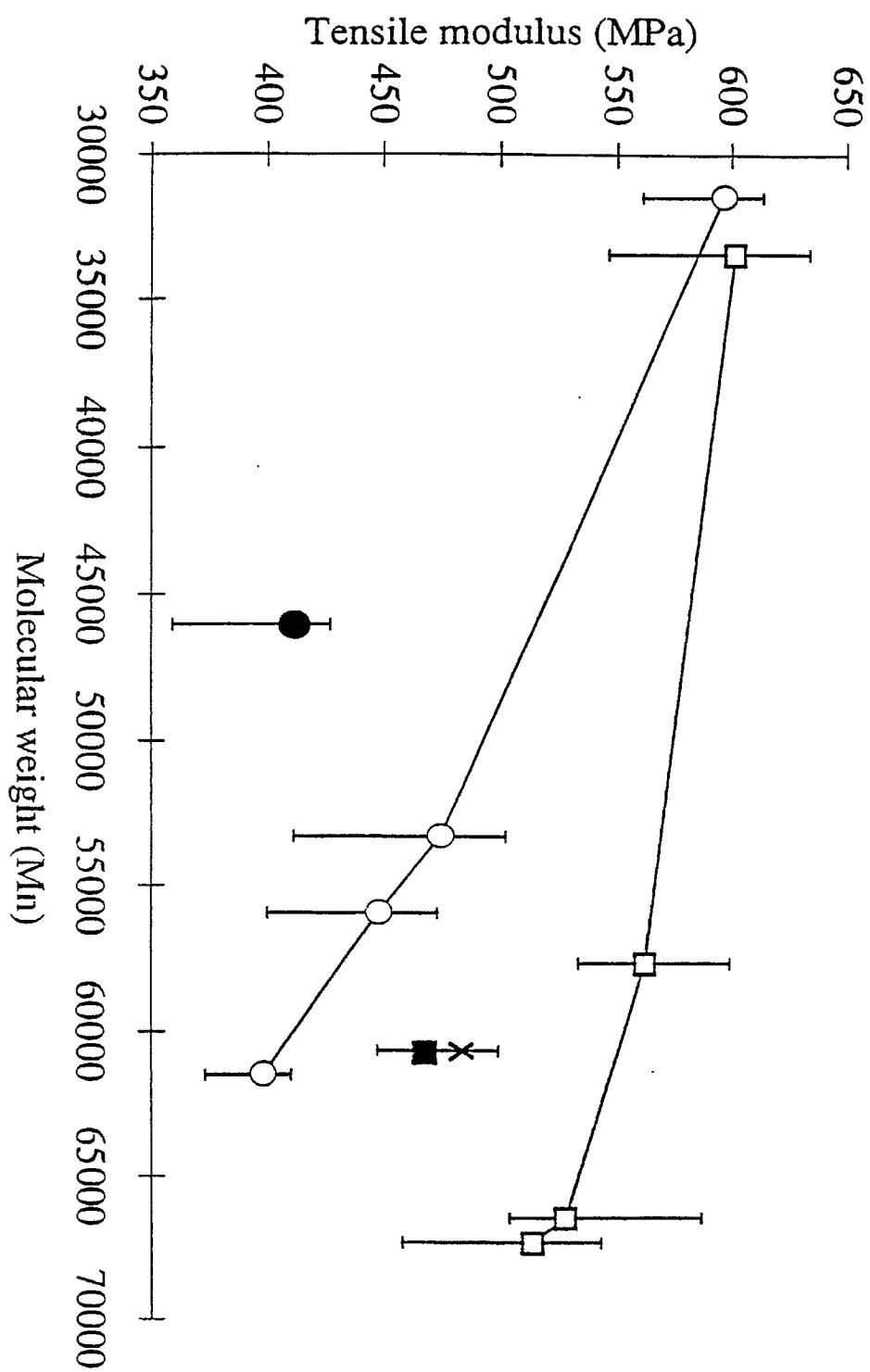


Figure 6

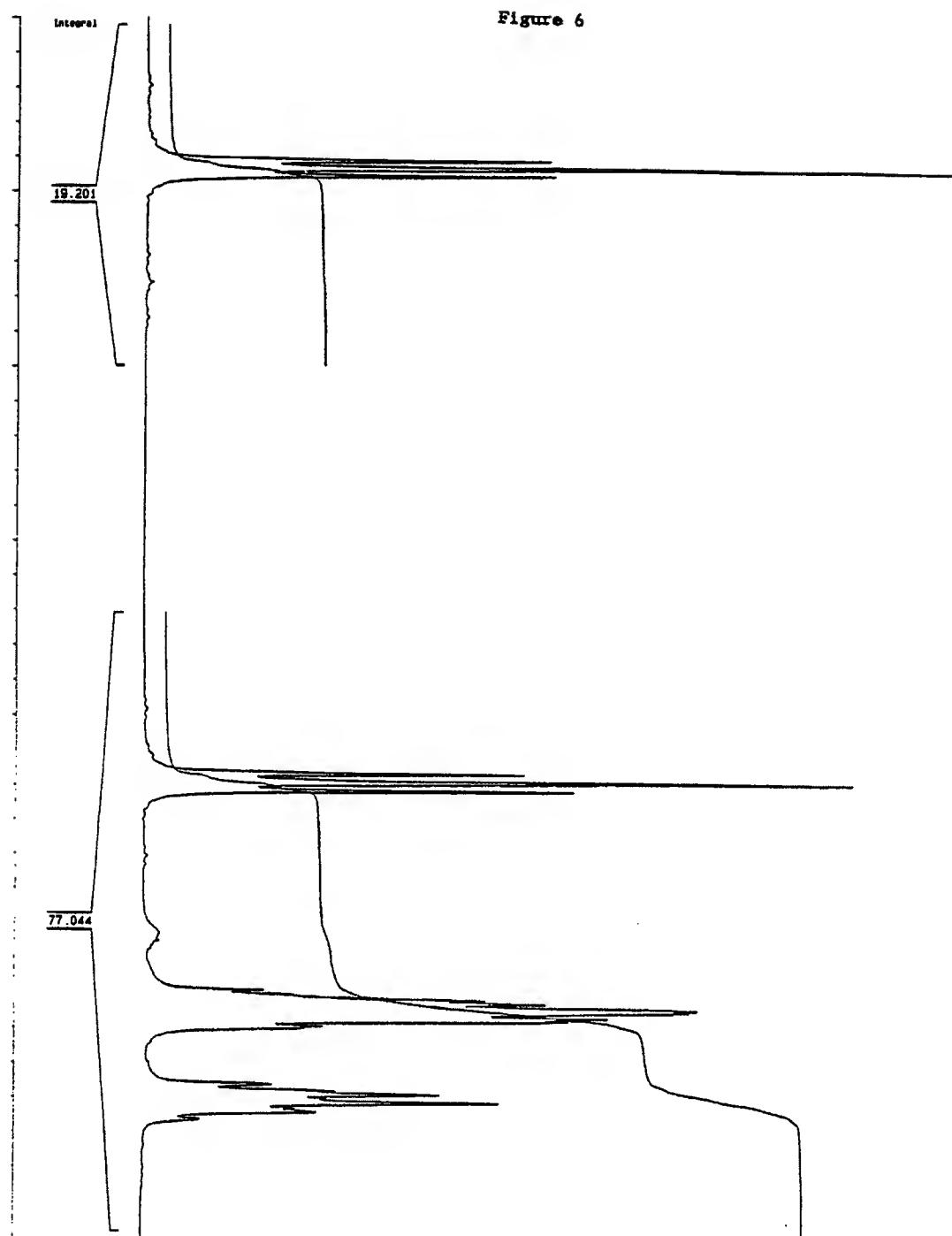


Figure 7

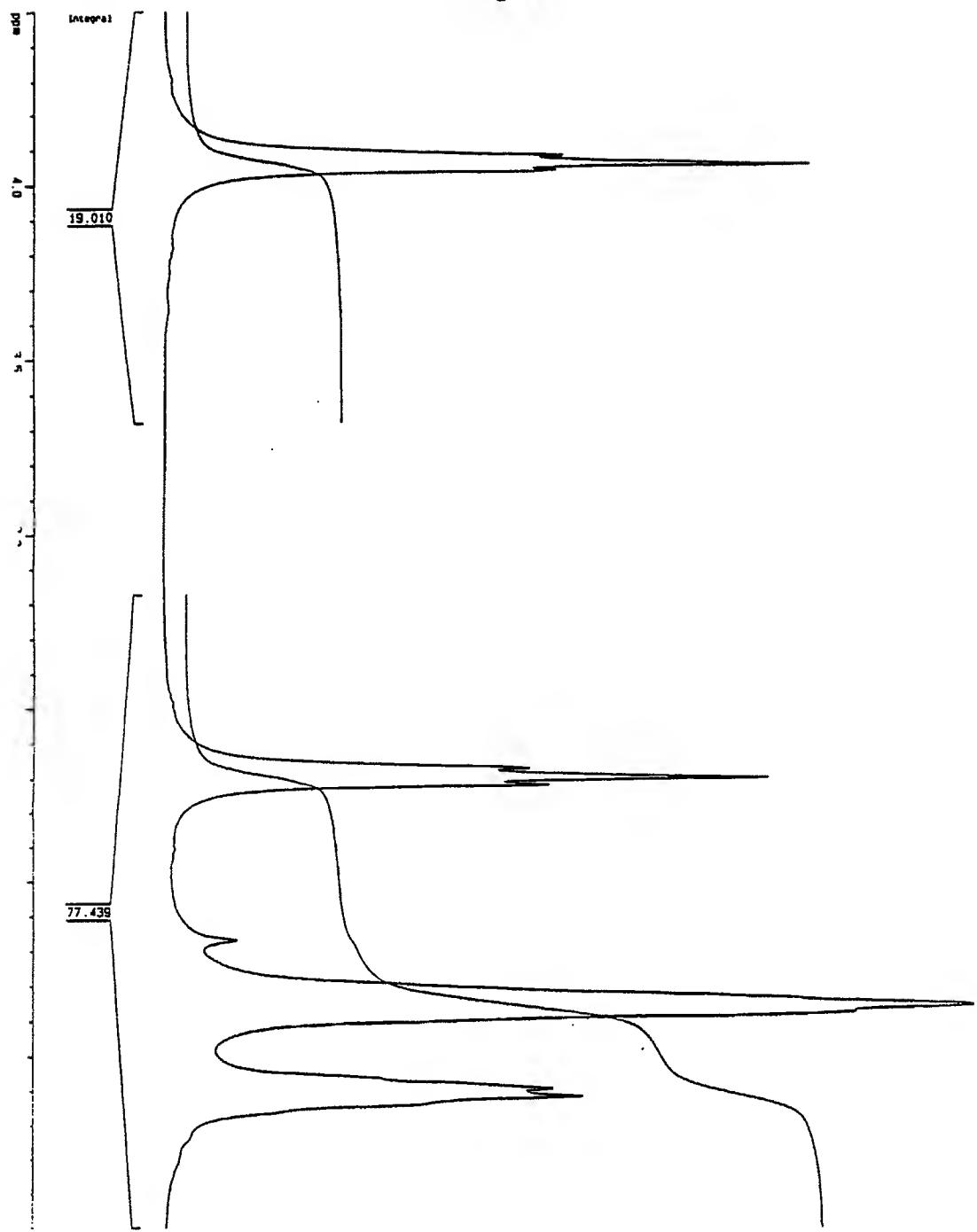
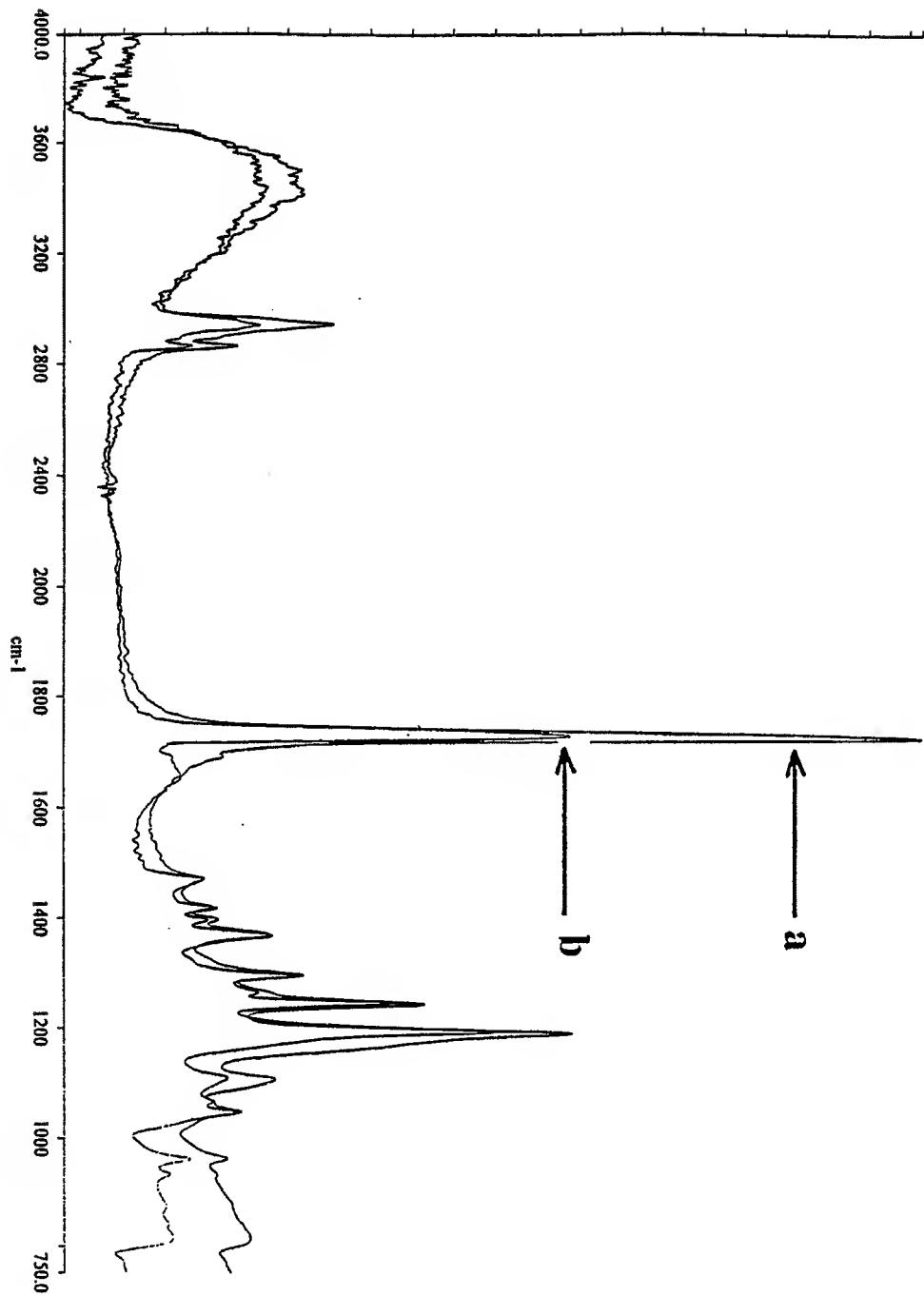


Figure 8

A



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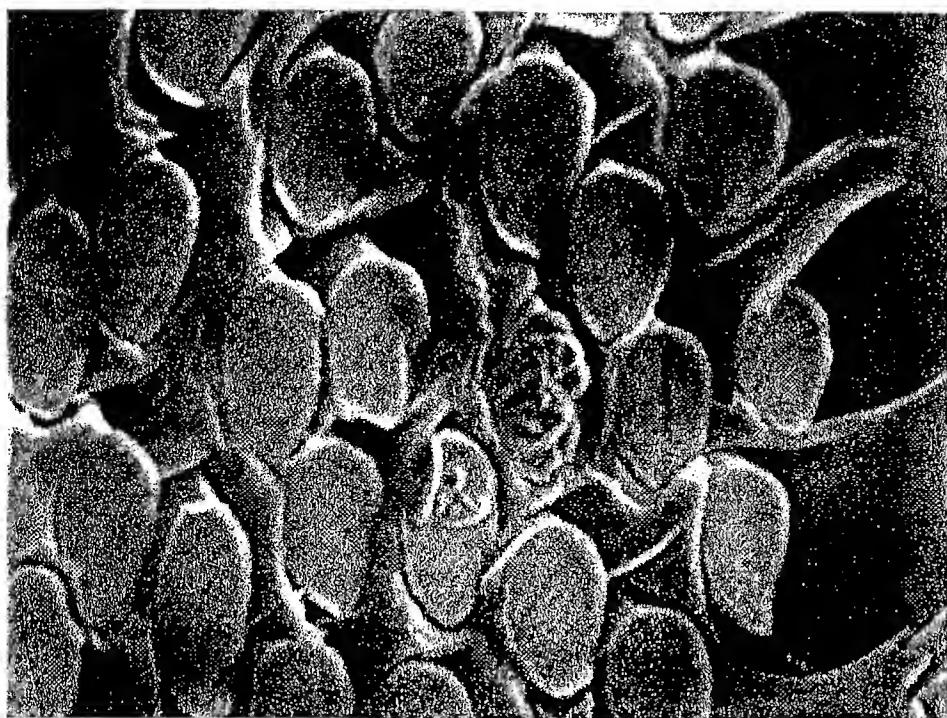


Fig 9

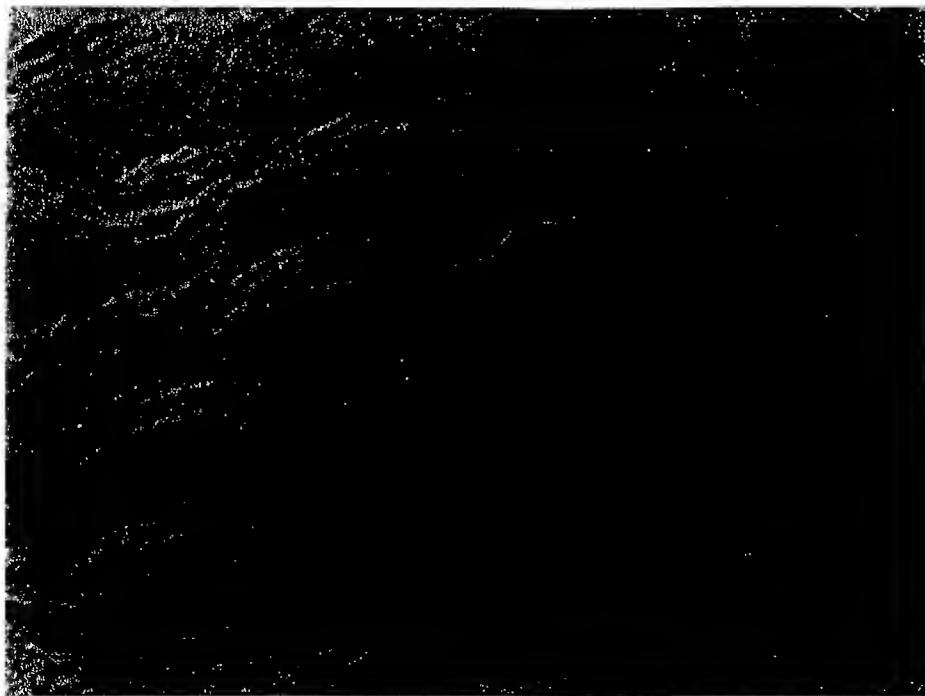


Fig 10



Fig 11

Activity of CFC on PCL of different molecular weights after 48 hours

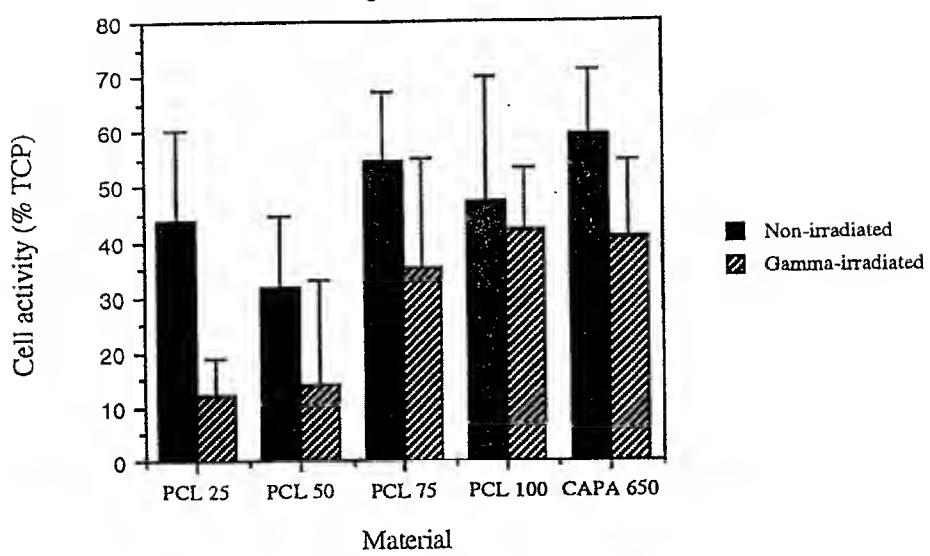


Fig 12